

2003PO4642WOUS
PCT/EP2004/003184

- 1 -

Description

TEMPERATURE MEASURING DEVICE AND REGULATION OF THE TEMPERATURE OF HOT GAS OF A GAS TURBINE

5

The invention relates to a gas turbine, in particular a stationary gas turbine for power generation, in accordance with the preamble of claim 1, and to a temperature-measuring device for recording the temperature of the air stream of a gas 10 turbine in accordance with the preamble of claim 5. The invention also relates to a control arrangement for controlling the hot-gas temperature of a gas turbine in accordance with the preamble of claim 6.

15 It is known that stationary gas turbines are used to generate mechanical energy, which a generator generally converts into electrical energy. For this purpose, a fossil fuel is burnt in the gas turbine with an air stream that has been compressed by the compressor, to form a hot gas which then expands so as to 20 perform work at the rotor in a turbine. The gas turbine is operated in such a way that sufficient energy is output at the rotor shaft to generate the electrical energy, while a maximum temperature of the hot gas at the turbine inlet should not be exceeded.

25

The turbine inlet temperature cannot be measured directly, on account of its high values. Therefore, the temperature of the exhaust gas which is present at the turbine outlet is recorded, and the turbine inlet temperature can then be determined by 30 calculation from this turbine outlet temperature. The turbine outlet temperature and therefore indirectly also the turbine inlet temperature can be controlled by means of the quantity of fuel introduced into the combustion chamber, while these temperatures are also dependent on the temperature of the air 35 at the compressor inlet. To simplify control of the gas

2003PO4642WOUS
PCT/EP2004/003184

- 1a -

turbine, an auxiliary variable is calculated by means of a mathematical model, eliminating the dependency of the turbine outlet temperature on the compressor inlet temperature.

This auxiliary variable is used as a corrected turbine outlet temperature. It is dependent only on the quantity of fuel consumed, resulting in simple control of the gas turbine. Although the control is also dependent on the mains frequency 5 of the power generated by the generator, this influence is not taken into account here.

To increase the performance of the gas turbine, it is also possible for water to be fed to the air stream sucked in by the 10 compressor even before it has been compressed, in order to increase the mass flow through the gas turbine. This is generally known as wet compression mode.

The temperature of the air which is sucked in generally differs 15 from the temperature of the liquid which is injected. Since the temperature-measuring devices arranged at the inlet of the compressor for measuring the air temperatures are wetted by the liquid that has been introduced, the temperature-measuring devices are not recording the temperature of the air, but 20 rather that of the liquid.

If, on account of a compressor inlet temperature which is clearly higher following the measurement, a lower turbine outlet temperature is determined than the turbine outlet 25 temperature which is actually present, the controller of the gas turbine increases the supply of fuel into the combustion chamber in order to compensate for the presumed difference. However, this leads to overfiring of the gas turbine, i.e. the actual turbine inlet temperature may become higher than the 30 maximum permissible turbine inlet temperature. The gas turbine is underfired if the compressor inlet temperature measured is lower than the actual turbine inlet temperature.

Overfiring of the gas turbine can lead to overheating of the 35 components exposed to hot gas and therefore to a reduction in

2003PO4642WOUS
PCT/EP2004/003184

- 2a -

their service life, or even to defects. On the other hand underfiring of the gas turbine leads to loss of performance.

The object of the invention is to provide a gas turbine in which the service life of the components exposed to hot gas is increased in wet compression mode yet nevertheless the maximum power output is achieved. A further object of the invention is 5 to provide a control arrangement which implements operation of this type. A further object of the invention is to provide a corresponding temperature-measuring device.

10 The object relating to the gas turbine is achieved by the features of claim 1. Advantageous configurations are given in the subclaims.

15 The solution provides for the temperature-measuring device to be arranged upstream of the injection apparatus, as seen in the direction of flow of the air, and for the temperature of the air stream at the compressor inlet to be calculated by means of the measured air temperature. Therefore, the liquid which is introduced cannot wet the temperature-measuring devices, which means that it is always the temperature of the air stream that 20 is sucked in which is measured. Simply protecting the temperature-measuring devices by means of protective tubes does not eliminate the problem, since in this case the temperature-measuring devices would measure the temperature of the protective tubes, and these tubes would in turn be wetted with 25 the liquid.

30 In an advantageous refinement, the humidity of the air stream can be determined by means of air-humidity-measuring devices upstream of the injection apparatus. If the air humidity and air temperature of the air stream that is sucked in are known, it is possible to determine the evaporation of the liquid which is introduced on its way to the compressor inlet. By taking the air humidity into account, it is possible for the temperature at the inlet of the compressor to be calculated particularly 35 accurately.

2003PO4642WOUS
PCT/EP2004/003184

- 3a -

If the temperature of the air stream at the compressor inlet is calculated by means of a function based on air temperature and

humidity distributions, this calculation is particularly simple.

In an advantageous refinement, the air temperature and humidity 5 distributions can be predetermined in the form of diagrams, so that it is particularly simple to portray the dependency of the evaporation of the injected liquid in the air stream. This contributes to simple calculation.

- 10 The object relating to the temperature-measuring device is achieved by the features of claim 5. The advantages of the temperature-measuring device suitably correspond to those of the gas turbine.
- 15 The object relating to the control arrangement is achieved by the features of claim 6. Advantageous configurations are given in the subclaims.

The solution provides for the temperature-measuring device to 20 be arranged upstream of the injection apparatus and for the air temperature of the air stream at the inlet of the compressor to be calculated by means of the measured temperature. The advantages of the control arrangement suitably correspond to those of the gas turbine.

25 In an advantageous configuration of the control arrangement, with 100% evaporation a minimum possible temperature is determined and used as replacement for the temperature at the inlet of the compressor. In this context, it is assumed that 30 the liquid introduced by the injection apparatus evaporates sufficiently for a relative air humidity of 100% to be established at the compressor inlet. Working on the basis of this assumption, it is possible, in conjunction with the measured air humidity and air temperature, to determine the 35 minimum feasible (lowest possible) temperature at the

compressor inlet. If the minimum possible temperature is now used as the temperature for the air stream at the compressor inlet, the temperature which actually prevails at the compressor inlet is always greater than

the minimum possible temperature, since an air humidity of 100% is never achieved without external action. In this situation, the gas turbine is always underfired. Overheating of the components exposed to hot gas is therefore avoided, so that the 5 service life of the components is not reduced.

An improved control arrangement for the gas turbine ensues if the temperature of the air stream at the inlet of the compressor is calculated taking account of the actual 10 evaporation of the injected liquid in the air stream. The efficiency of the evaporation is determined by calculations and/or tests, and this efficiency, with the aid of the minimum possible temperature, is used to determine the air temperature which is present at the compressor inlet. With this control 15 arrangement, it is possible to reproduce the true conditions with regard to evaporation of the introduced liquid on the way to the compressor inlet, and thereby to bring about reliable and more high-performance operation of the gas turbine, avoiding both overfiring and underfiring of the gas turbine.

20 In a preferred configuration of the control arrangement, the quantity of liquid injected into the air stream is altered as a function of the evaporation. The compressors of gas turbines are usually dimensioned for a predetermined quantity of liquid 25 which evaporates during the compression. However, the evaporation causes a small proportion of the injected liquid to evaporate even before the compression, which means that the compressor is not operated in the optimum range. This drawback can be avoided by adapting the quantity of liquid injected.

30 The efficiency of the evaporation, which is substantially dependent on the droplet characteristics and the geometry, i.e. the spatial arrangement of the components of a compressor, can be estimated from tests and/or determined from calculations, 35 which are then stored in the form of models or formulae in the controller. The avoidance of underfiring

increases the power output of the gas turbine, and the prevention of overfiring of the gas turbine means that the service life of the components which guide hot gas is not adversely affected.

5

The advantages of the control arrangement suitably correspond to the advantages of the gas turbine.

10 The invention is explained with reference to a drawing, in which:

Fig. 1 shows a gas turbine installation, and

15 Fig. 2 shows an intake housing of a gas turbine as shown in Fig. 1.

Fig. 1 diagrammatically depicts a gas turbine installation for converting fossil energy into electrical energy by means of a gas turbine 1 and a generator 2 coupled to it. The stationary 20 gas turbine 1 substantially comprises a compressor 3, a combustion chamber 5 and a turbine part 7. The compressor 3 is connected to the turbine part 7 and the generator 2 via a common rotor shaft 10.

25 When the gas turbine 1 is operating, the compressor 3 sucks in air through an intake housing 11 and compresses it. The compressed air is mixed with a fuel B, which can be supplied through a shut-off member 8, in a burner and fed to the combustion chamber 5. In operation, the mixture burns to form a 30 hot gas H which then flows into the turbine part 7, where the hot gas H expands and in so doing drives the rotor shaft 10. Then, the hot gas H leaves the gas turbine 1 as exhaust gas A, passing into an exhaust conduit (not shown in more detail). The rotor shaft 10 drives the compressor 3 and the generator 2.

To control operation of the gas turbine 1, the temperature T_{AT} of the hot gas H at the outlet 6 of the turbine part 7 is monitored by means of a temperature-measuring device M_{AT} , since the

Temperature T_{T1} of the hot gas H which is present at the inlet 14 of the turbine part 7 cannot be measured. Both the power of the gas turbine 1 and the turbine outlet temperature T_{AT} , and therefore indirectly also the turbine inlet temperature T_{T1} ,
5 can be controlled by the quantity of fuel B introduced into the combustion chamber 5. An increase in the volumetric flow of the fuel B into the gas turbine 1 leads to a higher temperature of the hot gas H and to an increase in the power of the gas turbine 1. For this purpose, the controller 13 controls the
10 shut-off member 8, which it actuates via its outlet.

Since the turbine inlet temperature T_{T1} is also dependent on the temperature T_{v1} of the air stream L which is sucked in upstream of the compressor 3, this temperature is likewise
15 recorded or determined constantly, i.e. at recurring intervals throughout the entire duration of operation.

The controller 13 eliminates the dependency of the turbine outlet temperature T_{AT} on the air temperature T_{v1} by determining
20 a corrected turbine outlet temperature T_{ATK} as auxiliary variable in accordance with the following equation

$$T_{ATK} = T_{AK} - k_1 \cdot T_{v1} \quad (1).$$

25 Accordingly, the corrected turbine outlet temperature T_{ATK} is dependent only on the fuel B which is introduced, so that the gas turbine 1 can be controlled more easily by controlling the corrected turbine outlet temperature T_{ATK} as a control variable and setting the volumetric flow of the fuel B as manipulated
30 variable. The corrected turbine outlet temperature T_{ATK} could also be determined on the basis of a quadratic equation or on the basis of other functions.

The controller 13 has an input, at which the desired value T_{soll}
35 of the corrected turbine outlet temperature can be set. In the

2003PO4642WOUS
PCT/EP2004/003184

- 7a -

controller 13, the desired value T_{S011} is compared with the determined corrected turbine outlet temperature T_{ATK} . If the actual value, the corrected turbine outlet

temperature T_{ATK} is lower - higher - than the desired value T_{sol1} , the controller 13 uses the shut-off member 8 to increase - reduce - the supply of fuel.

- 5 If the gas turbine 1 is operated without a liquid being introduced into the air stream L, the temperature-measuring device M_{LU} arranged upstream of the intake housing 11 can measure the temperature T_{v1} of the air stream at the compressor inlet 12 directly.

10

- Fig. 2 shows the intake housing 11 of the gas turbine 1. The temperature-measuring devices M_{TU} are arranged above an injection apparatus 9, so that the liquid W which is introduced does not wet the temperature-measuring devices M_{TU} and the air-humidity-measuring devices M_{FU} .

15

In wet compression mode, a liquid W, in particular water, is injected into the air stream L sucked in in the intake housing 11 via the injection apparatus 9.

20

- The temperature T_u of the air which is sucked in is determined upstream of the intake housing 11 by means of the temperature-measuring devices M_{LU} , and the air humidity F_u of this air is determined upstream of the intake housing 11 by means of the air-humidity-measuring devices M_{FU} . The outputs of these measuring devices are connected to the inputs of the controller 13.

30

The temperature T_{v1} which is present at the inlet 12 of the compressor 3 and is required for control is determined as a function of the measured values and on the basis of models in the controller 13. Therefore, the gas turbine 1 can be controlled by controlling the turbine outlet temperature T_{ATK} by means of the quantity of fuel B injected using equation (1).

If it is intended for the gas turbine 1 to be operated with injection of a liquid W into the air stream L sucked in by the compressor 3, two different control arrangements are possible:

control with a theoretical evaporation which leads to an assumed air humidity of 100%, and adapted control with variable evaporation.

- 5 In the case of the control with the theoretical evaporation, it
is assumed that enough of the injected liquid has evaporated
for the air humidity in the intake air stream L at the
compressor inlet 12 to be 100%. On this assumption, a minimum
feasible temperature $T_{WetBulb}$, which replaces the temperature T_{v1}
10 at the compressor inlet 12, is determined on the basis of the
measured temperature T_u and air humidity F_u of the air stream
L. The compressor inlet temperature T_{v1} determined in this way
can be ascertained by calculation or also from diagrams which
are reproduced in electronic form in measurement technology, or
15 also by means of mathematical formulae. The equation for the
controller 13 for determining the corrected turbine outlet
temperature T_{ATK} is then as follows:

$$T_{ATK} = T_{AK} - k_1 \cdot T_{WetBulb} \quad (2).$$

- 20 Since an air humidity of 100% is never achieved in real
operation, the actual temperature T_{v1} at the inlet 12 of the
compressor 3 is always greater than the assumed minimum
feasible temperature. The use of the minimum feasible
25 compressor inlet temperature $T_{WetBulb}$ in each case determines an
excessively high corrected turbine outlet temperature T_{ATK} , so
that the controller 13 always provides an insufficient quantity
of fuel B to the burner. This prevents overfiring of the gas
turbine 1. Accordingly, the components of the gas turbine 1
30 which are exposed to hot gas, such as turbine blades and vanes,
guide rings, platforms and combustion chamber heat shields, are
exposed to the appropriate temperatures and premature fatigue
is prevented in these components.

- 35 In the case of the adapted control of the gas turbine 1, an air

humidity which is present at the inlet 12 of the compressor 3 is determined, although this air humidity is lower than 100% and

can be determined as a function of the measured air humidity F_u , the measured temperature T_u of the air stream L and the quantity of liquid W introduced by the injection apparatus 9. The efficiency η of the evaporation of the liquid W in the 5 intake air stream L is also taken into account in this calculation in order to determine the temperature T_{v1} at the inlet 12 of the compressor 3.

The efficiency of saturation of the air stream L with a liquid 10 W can be calculated according to

$$\eta = \frac{T_u - T_{v1}}{T_u - T_{WetBulb}} \quad (3).$$

Resolving equation (3) with respect to T_{v1} and then inserting 15 it into equation (1) gives:

$$T_{ATK} = T_{AT} - k_1 \cdot [T_u - \eta \cdot (T_u - T_{WetBulb})] \quad (4).$$

The efficiency η of the evaporation, which is dependent on the 20 droplet characteristics of the injected water and on the geometry, i.e. the spatial arrangement of the components of the compressor 3, can be determined by calculation and/or by tests and is then stored on the basis of a model or a diagram in electronic form in the controller 13.

25 Evaporation of the liquid W which leads to an air humidity at the inlet 12 of the compressor 3 which is lower than 100% gives a better description of the real conditions, resulting in improved control of the gas turbine 1.

30 A corrected turbine outlet temperature (T_{ATK}) determined in accordance with equation (4) is lower than a corrected turbine outlet temperature T_{ATK} determined on the basis of equation (2), so that power losses resulting from the turbine inlet 35 temperature T_{T1} being assumed to be too low are avoided.

Furthermore, it is possible to determine the quantity of liquid W which evaporates before it reaches the inlet 12 into the compressor 3, and this quantity is then additionally injected by the injection apparatus 1. This leads to a further increase 5 in the power of the gas turbine 1, since only the proportion of the liquid (W) which evaporates during the compression - i.e. in the compressor 3 - contributes to increasing the power of the gas turbine 1 by wet compression.